INVERSE HEAT TRANSFER PROBLEMS

Helcio R. B. Orlande

Department of Mechanical Engineering
Escola Politécnica/COPPE
Federal University of Rio de Janeiro, UFRJ
Rio de Janeiro, RJ, Brazil
helcio@mecanica.coppe.ufrj.br





In cooperation with

George Dulikravich (Florida International University – USA)

Marcelo Colaço (COPPE/UFRJ – Brazil)

Olivier Fudym (Ecole des Mines D'Albi – France)

Renato Cotta (COPPE/UFRJ – Brazil)

Carolina Naveira-Cotta (COPPE/UFRJ – Brazil)

Jean-Luc Battaglia (TREFLE/Bordeaux – France)

Jari Kaipio (University of Auckland – New Zealand)

Ville Kolehmainen (University of Eastern Finland – Finland)

Markus Neumayer (Graz University of Technology – Austria)

Daniel Watzenig (Graz University of Technology – Austria)

Carlos Alves (Instituto Superior Técnico – Lisbon)

Nilson Roberty (COPPE/UFRJ – Brazil)

Henrique M. da Fonseca (COPPE/UFRJ – Brazil)

Bernard Lamien (COPPE/UFRJ – Brazil)

Diego Knupp (COPPE/UFRJ – Brazil)

Luiz Abreu (COPPE/UFRJ – Brazil)



OUTLINE

- INTRODUCTION
- SOLUTION OF INVERSE PROBLEMS
- > General considerations
- > Bayesian framework: MCMC, PARTICLE FILTER
 - Computational speed-up
 - Improvement of solutions with reduced models
- CONCLUSIONS



INTRODUCTION

Inverse heat transfer problems deal with the estimation of unknown quantities appearing in the mathematical formulation of physical processes in thermal sciences, by using measurements of temperature, heat flux, radiation intensities, etc.



INTRODUCTION

- Originally, inverse heat transfer problems have been associated with the estimation of an unknown boundary heat flux, by using temperature measurements taken below the boundary surface of a heat conducting medium.
- Recent technological advancements often require the use of involved experiments and indirect measurements, within the research paradigm of inverse problems.
- Nowadays, inverse analyses are encountered in single and multimode heat transfer problems, dealing with multi-scale phenomena.
- Applications range from the estimation of constant heat transfer parameters to the mapping of spatially and timely varying functions, such as heat sources, fluxes and thermophysical properties.



SOLUTION OF INVERSE PROBLEMS General Considerations

Consider the mathematical formulation of a heat transfer problem, which, for instance, can be linear or non-linear, one or multi-dimensional, involve one single or coupled heat transfer modes, etc.

We denote the **vector of parameters** appearing in such formulation as:

$$\mathbf{P}^T = [P_1, P_2, ..., P_N]$$

where N is the number of parameters

- These parameters can possibly be thermal conductivity components, heat transfer coefficients, heat sources, boundary heat fluxes, etc.
- They can represent constant values of such quantities, or the parameters of the representation of a function in terms of known basis functions.



General Considerations

Consider also that transient measurements are available within the medium, or at its surface, where the heat transfer processes are being mathematically formulated.

The vector containing the **measurements** is written as:

$$\mathbf{Y}^T = \left(\vec{Y}_1, \vec{Y}_2, \dots, \vec{Y}_I\right)$$

$$\vec{Y}_i = (Y_{i1}, Y_{i2}, \dots, Y_{iM})$$

$$M = \#$$
 of sensors $I = \#$ of transient measurements per sensor

$$D = MI = \#$$
 of measurements

• The measured data are not limited to temperatures, but could also include heat fluxes, radiation intensities, etc.



The <u>statistical inversion approach</u> is based on the following principles (Jari P. Kaipio and Erkki Somersalo, *Computational and Statistical Methods for Inverse Problems*, Springer, 2004):

- 1. All variables included in the formulation are modeled as random variables.
- 2. The randomness describes the degree of information concerning their realizations.
- 3. The degree of information concerning these values is coded in the probability distributions.
- 4. The solution of the inverse problem is the posterior probability distribution.



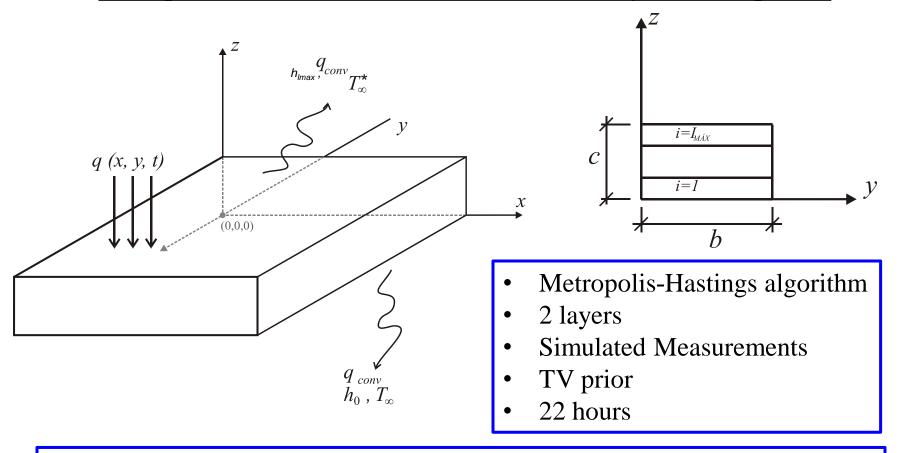
- In many cases, the Posterior Probability Distribution does not allow an analytical treatment.
- Draw samples from the set Ω of all possible **P**'s, each sample with probability $\pi(\mathbf{P}|\mathbf{Y})$.
- Get a set $\Theta = \{\mathbf{P}_1, \mathbf{P}_2, ..., \mathbf{P}_M\}$ of samples distributed like the posterior distribution.
- Inference on $\pi(\mathbf{P}|\mathbf{Y})$ becomes inference on $\Theta = \{\mathbf{P}_1, \mathbf{P}_2, ..., \mathbf{P}_M\}$, for example the mean of the samples in Θ give us an estimation of the average values of $\pi(\mathbf{P}|\mathbf{Y})$.
- We generally need the constant that normalizes the probability distribution:

 MARKOV CHAIN MONTE-CARLO METHODS

 (Metropolis-Hastings Algorithm)
- Very time consuming.



Example: Estimation of Contact Failures in Layered Composites



L. A. Abreu, H. R. B. Orlande, J. Kaipio, V. Kolehmainen, R. M. Cotta, J. N. N. Quaresma, Identification Of Contact Failures In Multi-layered Composites With The Markov Chain Monte Carlo Method, ASME *Journal of Heat Transfer*, (under review)

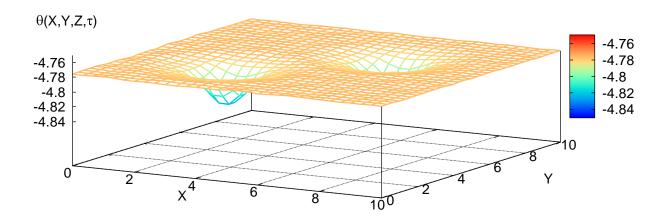


Figure 5.a Exact temperature distribution at Z = 1 and $\tau = 0.065$ – two square failures of size 0.005 m

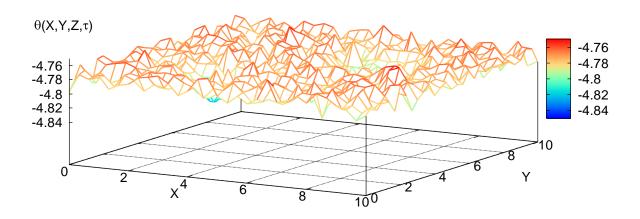
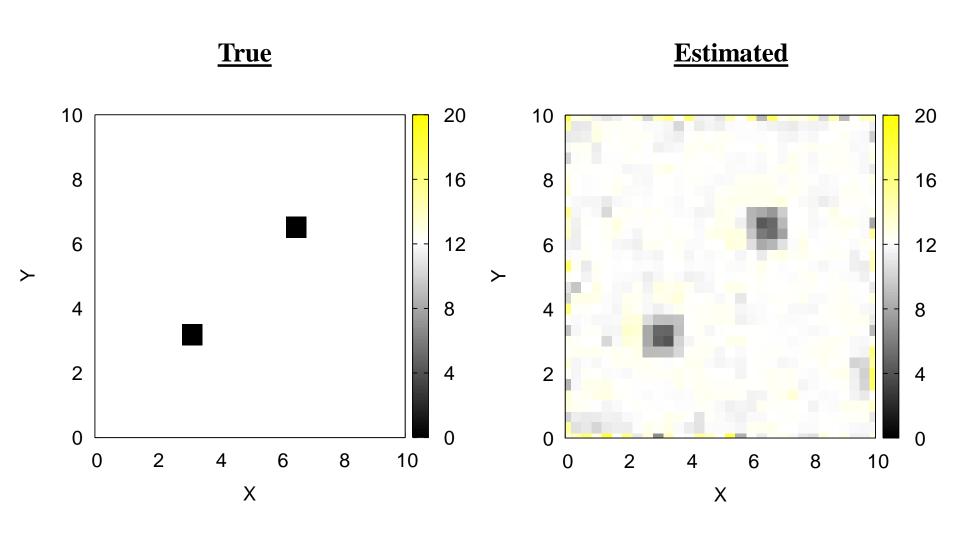


Figure 5.b Simulated measurements at Z = 1 and $\tau = 0.065$ – two square failures of size 0.005





Example: Estimation of Thermal Conductivity Components of Orthotropic Solids

$$k_1 \frac{\partial^2 T}{\partial x^2} + k_2 \frac{\partial^2 T}{\partial y^2} + k_3 \frac{\partial^2 T}{\partial z^2} = \frac{\partial T}{\partial t} \quad \text{in } 0 < x < a, \ 0 < y < b, \ 0 < z < c; \ t > 0$$

$$T = 0$$
 at $x = 0$; $k_1 \frac{\partial T}{\partial x} = q_1(t)$ at $x = a$, for $t > 0$

$$T = 0$$
 at $y = 0$; $k_2 \frac{\partial T}{\partial y} = q_2(t)$ at $y = b$, for $t > 0$

$$T = 0$$
 at $z = 0$; $k_3 \frac{\partial T}{\partial z} = q_3(t)$ at $z = c$, for $t > 0$

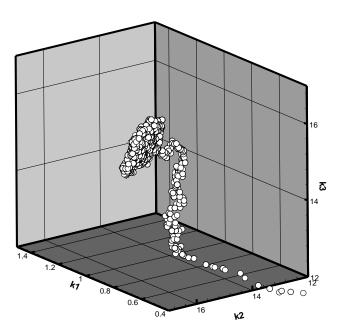
$$T = 0$$
 for $t = 0$; in $0 < x < a$, $0 < y < b$, $0 < z < c$

Orlande, H.R.B., Colaço, M., Dulikravich, G., Approximation of the likelihood function in the Bayesian technique for the solution of inverse problems, *Inverse Problems in Science and Engineering*, Vol. 16, pp. 15 677–692, 2008.

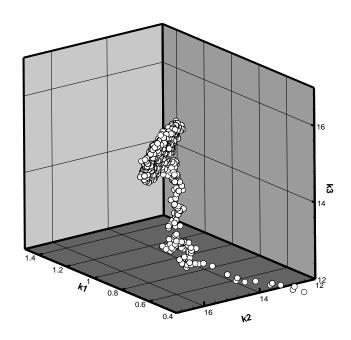


Bayesian framework

Example: Estimation of Thermal Conductivity Components of Orthotropic Solids – Interpolation of the Likelihood with RBF's



Exact Likelihood (48 seconds)

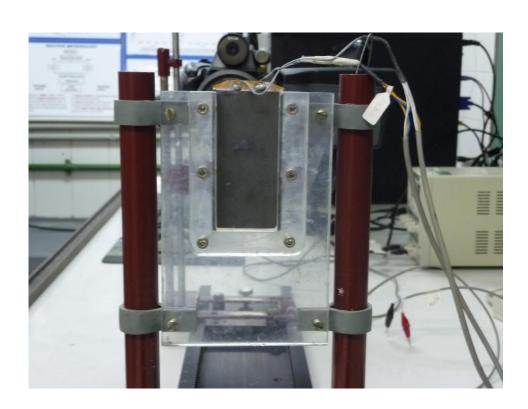


Interpolated Likelihood (1.8 seconds)

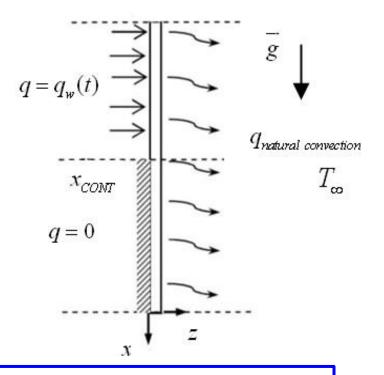
Orlande, H.R.B., Colaço, M., Dulikravich, G., Approximation of the likelihood function in the Bayesian technique for the solution of inverse problems, *Inverse Problems in Science and Engineering*, Vol. 16, pp. 16 677–692, 2008.



Example: Characterization of Heterogeneous Media



Thin plate: Lumped model in z

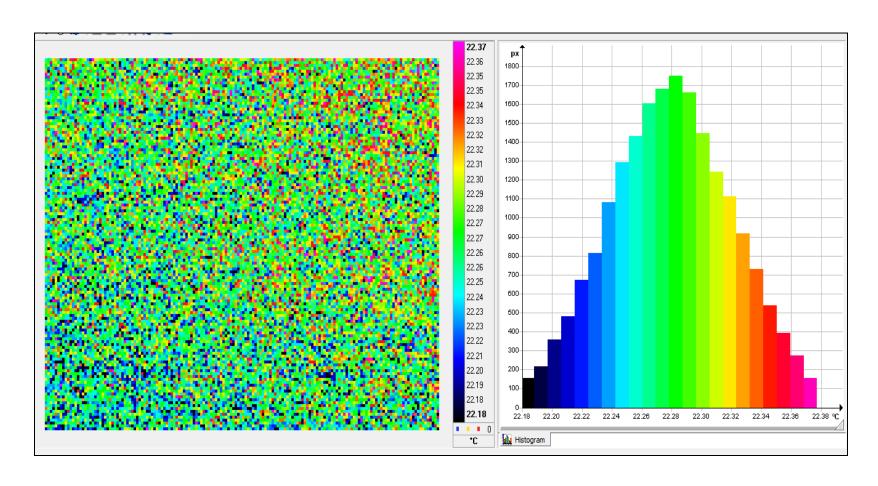


Orlande, H. R. B., Knupp, D., Naveira-cotta, C., Cotta, Renato, Experimental Identification of Thermophysical Properties in Heterogeneous Materials with Integral Transformation of Temperature Measurements from Infrared Thermography. *Experimental Heat Transfer.*, v.26, p.1 - 25, 2013.



Bayesian framework

YES! The likelihood is Gaussian!





Example: Characterization of Heterogeneous Media

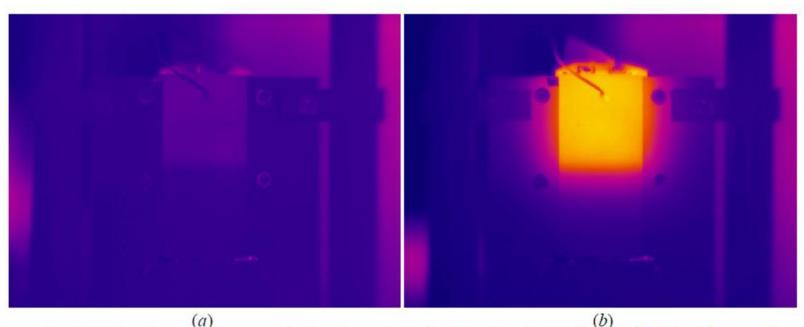
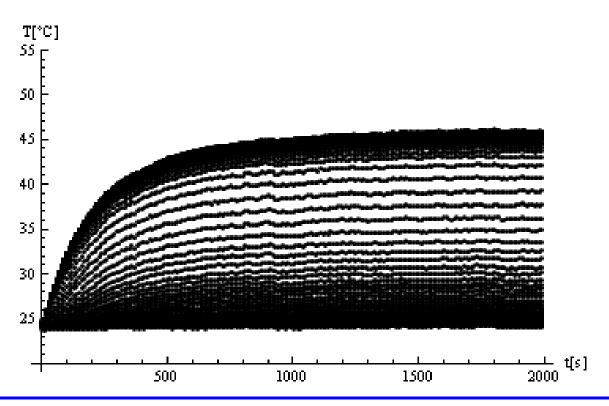


Figure 7 – (a) Infrared camera image acquired at the moment the DC source is switched on. (b) Infrared camera image acquired after some elapsed time during heating period.

Orlande, H. R. B., Knupp, D., Naveira-cotta, C., Cotta, Renato, Experimental Identification of Thermophysical Properties in Heterogeneous Materials with Integral Transformation of Temperature Measurements from Infrared Thermography. *Experimental Heat Transfer.*, v.26, p.1 - 25, 2013.



Example: Characterization of Heterogeneous Media



The number of pixels in the vertical direction for the configuration that has been tested provides the total number of 328 spatial measurements along the 8 cm of the plate.



Example: Characterization of Heterogeneous Media <u>Data Compression</u>

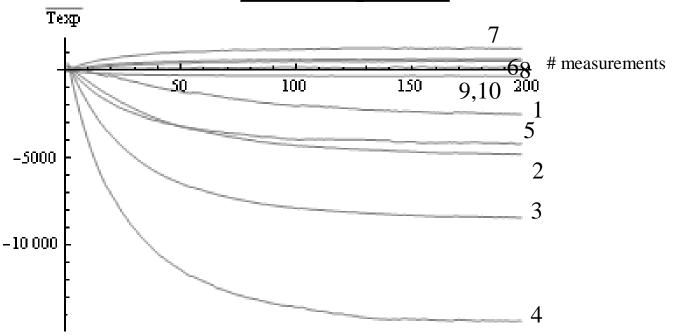
Another advancement of the present study was the solution of the inverse problem in the transformed field, from the integral transformation of the experimental temperature data, thus compressing the experimental measurements in the space variables into a few transformed fields. Once the experimental temperature readings have been obtained, one proceeds to the integral transformation of the temperature field at each time through the integral transform pair below:

Transform
$$\overline{T_{\exp,i}}(t) = \int_{0}^{Lx} w(x) \tilde{\psi}_{i}(x) [T_{\exp}(x,t) - T_{\infty}] dx$$
Inverse
$$T_{\exp}(x,t) = T_{\infty} + \sum_{i=0}^{Ni} \tilde{\psi}_{i}(x) \overline{T_{\exp,i}}(t)$$

Orlande, H. R. B., Knupp, D., Naveira-cotta, C., Cotta, Renato, Experimental Identification of Thermophysical Properties in Heterogeneous Materials with Integral Transformation of Temperature Measurements from Infrared Thermography. *Experimental Heat Transfer.*, v.26, p.1 - 25, 2013.



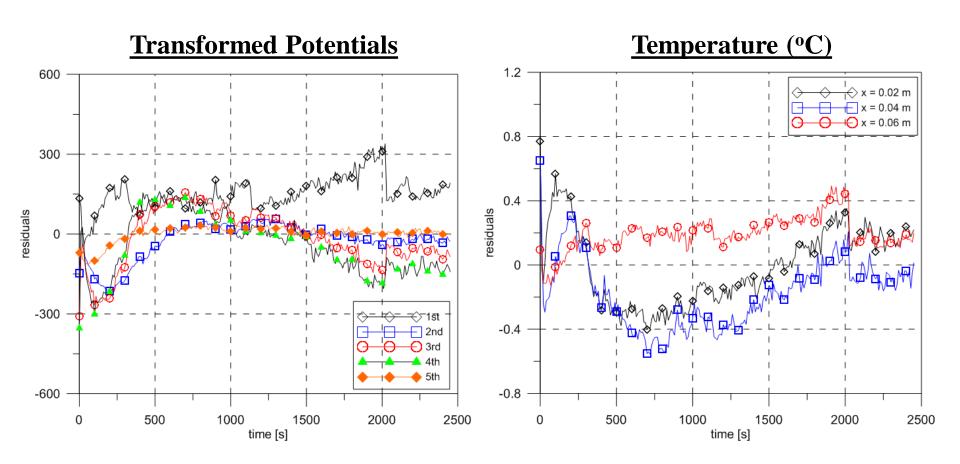
Example: Characterization of Heterogeneous Media <u>Data Compression</u>



These are in fact the quantities that are employed in the inverse problem analysis. Therefore, a significant data reduction of more than 95% is achieved, as one chooses to solve the inverse problem in the transformed 22 temperature domain.



Bayesian framework



Orlande, H. R. B., Knupp, D., Naveira-cotta, C., Cotta, Renato, Experimental Identification of Thermophysical Properties in Heterogeneous Materials with Integral Transformation of Temperature Measurements from Infrared Thermography. *Experimental Heat Transfer.*, v.26, p.1 - 25, 2013.



Bayesian framework

Example: Characterization of Heterogeneous Media – Nodal Approach

Thin plate: Lumped model in z

$$C(x,y)\frac{\partial T}{\partial t} = \frac{\partial}{\partial x} \left[k(x,y)\frac{\partial T}{\partial x} \right] + \frac{\partial}{\partial y} \left[k(x,y)\frac{\partial T}{\partial y} \right] - h(x,y) \left(T - T_{\infty} \right) + g(x,y)$$

By writing the equation above in non-conservative form:

$$\frac{\partial T}{\partial t} = a(x, y) \nabla^2 T + \frac{1}{C(x, y)} \left[\frac{\partial k(x, y)}{\partial x} \frac{\partial T}{\partial x} + \frac{\partial k(x, y)}{\partial y} \frac{\partial T}{\partial y} \right] - H(x, y) (T - T_{\infty}) + G(x, y)$$

$$a(x, y) = \frac{k(x, y)}{C(x, y)}$$

$$a(x,y) = \frac{k(x,y)}{C(x,y)}$$

$$H(x,y) = \frac{h(x,y)}{C(x,y)}$$

$$G(x, y) = \frac{g(x, y)}{C(x, y)}$$

Massard, H., Fudym, O., Orlande, H. R. B., Batsale, J. C., Nodal predictive error model and Bayesian approach for thermal diffusivity and heat source mapping, Comptes Rendus Mécanique, v.338, p.434 - 449, 2010



Example: Characterization of Heterogeneous Media – Nodal Approach

$$\mathbf{Y}_{ij} = \mathbf{J}_{ij} \mathbf{P}_{ij}$$

$$\mathbf{J}_{ij} = \begin{bmatrix} L_{i,j}^{1} & Dx_{i,j}^{1} & Dy_{i,j}^{1} & -\Delta t (T_{i,j}^{1} - T_{\infty}) & \Delta t \\ L_{i,j}^{2} & Dx_{i,j}^{2} & Dy_{i,j}^{2} & -\Delta t (T_{i,j}^{2} - T_{\infty}) & \Delta t \\ \vdots & \vdots & \vdots & \vdots & \vdots \\ L_{i,j}^{n_{t}} & Dx_{i,j}^{n_{t}} & Dy_{i,j}^{n_{t}} & -\Delta t (T_{i,j}^{n_{t}} - T_{\infty}) & \Delta t \end{bmatrix} \qquad \mathbf{Y}_{ij} = \begin{bmatrix} Y_{i,j}^{1} \\ Y_{i,j}^{2} \\ \vdots \\ Y_{i,j}^{n_{t}} \end{bmatrix}$$

$$\mathbf{Y}_{ij} = egin{bmatrix} Y_{i,j}^1 \ Y_{i,j}^2 \ dots \ Y_{i,j}^{n_t} \end{bmatrix}$$

$$\mathbf{P}_{ij} = egin{bmatrix} a_{i,j} \ \delta^x_{i,j} \ \delta^y_{i,j} \ H_{i,j} \ G_{i,j} \end{bmatrix}$$

In the nodal strategy, the sensitivity matrix is approximately computed with the measurements:

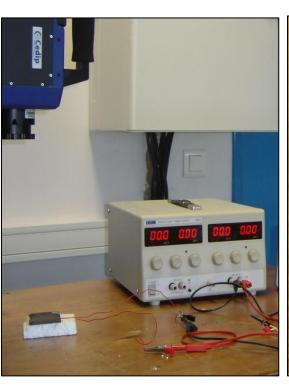
$$\pi(\mathbf{P},\mathbf{J}|\mathbf{Y}) \propto \pi(\mathbf{Y}|\mathbf{P},\mathbf{J})\pi(\mathbf{P})\pi(\mathbf{J})$$

Massard, H., Fudym, O., Orlande, H. R. B., Batsale, J. C., Nodal predictive error model and Bayesian approaches for thermal diffusivity and heat source mapping, Comptes Rendus Mécanique, v.338, p.434 - 449, 2010

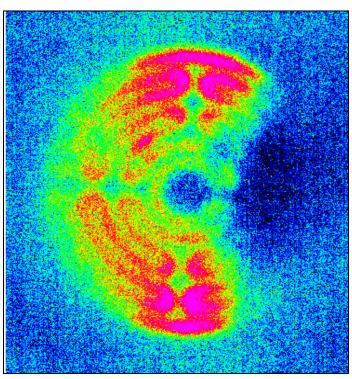


Bayesian framework

Example: Characterization of Heterogeneous Media - Nodal Approach

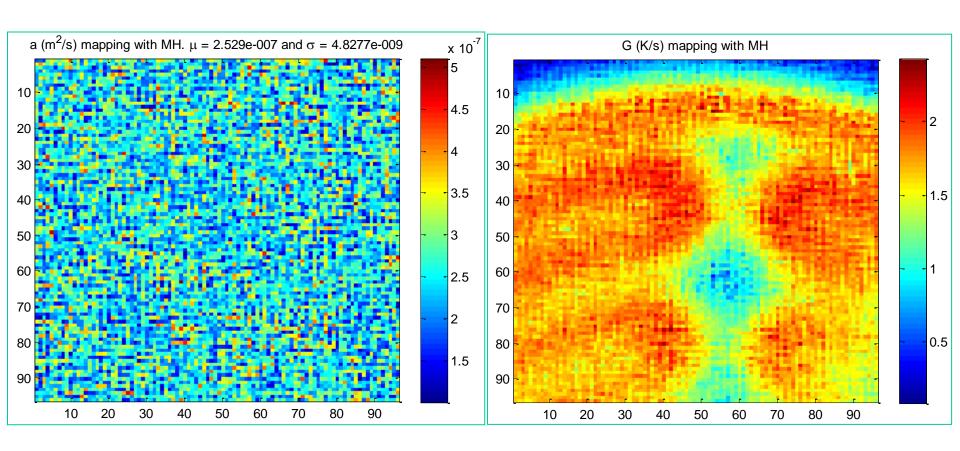








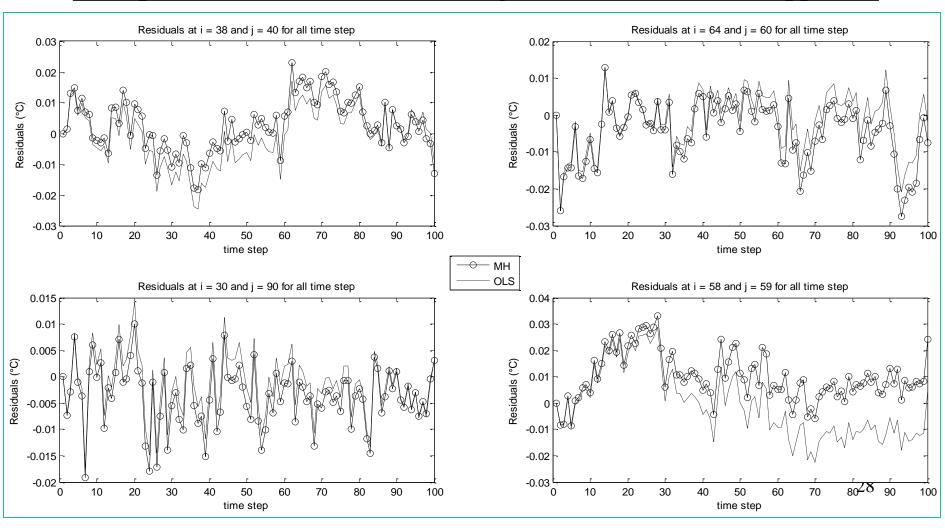
Example: Characterization of Heterogeneous Media – Nodal Approach





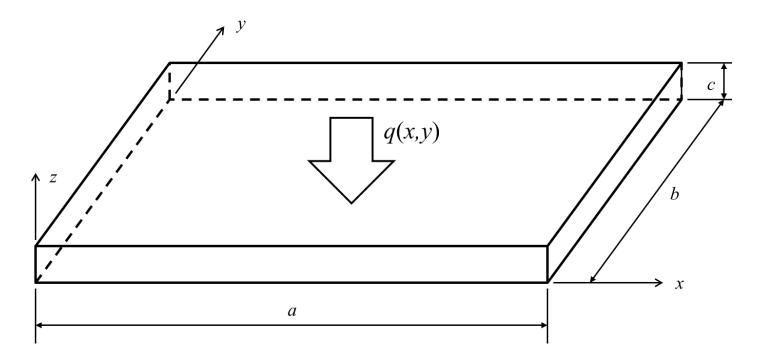
Bayesian framework

Example: Characterization of Heterogeneous Media – Nodal Approach

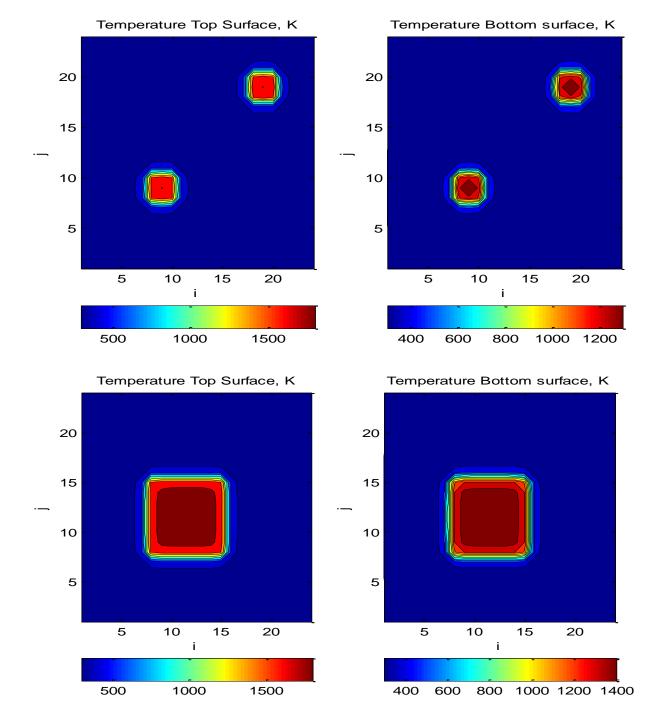




Example: Non linear 3D heat conduction Estimation of q(x,y) with measurements of T(x,y,0,t)



Helcio R. B. Orlande, George S. Dulikravich, Markus Neumayer, Daniel Watzenig, Marcelo J. Colaço, Accelerated Bayesian Inference For The Estimation Of Spatially Varying Heat Flux In A Heat Conduction Problem, *Numerical Heat Transfer – Part A*, In press





Complete model

$$C(T_c) \frac{\partial T_c(x, y, z, t)}{\partial t} = \frac{\partial}{\partial x} \left[k(T_c) \frac{\partial T_c}{\partial x} \right] + \frac{\partial}{\partial y} \left[k(T_c) \frac{\partial T_c}{\partial y} \right] + \frac{\partial}{\partial z} \left[k(T_c) \frac{\partial T_c}{\partial z} \right]$$

$$\text{in } 0 < x < a \text{ , } 0 < y < b \text{ , } 0 < z < c \text{ , for } t > 0$$

$$\frac{\partial T_c}{\partial x} = 0 \qquad \text{at } x = 0 \text{ and } x = a \text{ , } 0 < y < b \text{ , } 0 < z < c \text{ , for } t > 0$$

$$\frac{\partial T_c}{\partial y} = 0 \qquad \text{at } y = 0 \text{ and } y = b \text{ , } 0 < x < a \text{ , } 0 < z < c \text{ , for } t > 0$$

$$\frac{\partial T_c}{\partial z} = 0 \qquad \text{at } z = 0 \text{ , } 0 < x < a \text{ , } 0 < y < b \text{ , for } t > 0$$

$$k(T_c) \frac{\partial T_c}{\partial z} = q(x, y) \qquad \text{at } z = c \text{ , } 0 < x < a \text{ , } 0 < y < b \text{ , for } t > 0$$

$$T_c = T_0 \qquad \text{for } t = 0 \text{ , in } 0 < x < a \text{ , } 0 < y < b \text{ , } 0 < z < c$$



Reduced models: Linear problem with properties at T^*

$$C^* \frac{\partial \overline{T}(x, y, t)}{\partial t} = \frac{\partial}{\partial x} \left[k^* \frac{\partial \overline{T}}{\partial x} \right] + \frac{\partial}{\partial y} \left[k^* \frac{\partial \overline{T}}{\partial y} \right] + \frac{q(x, y)}{c}$$
in $0 < x < a$, $0 < y < b$, for $t > 0$

$$\frac{\partial \overline{T}}{\partial x} = 0 \qquad \text{at } x = 0 \text{ and } x = a, 0 < y < b, \text{ for } t > 0$$

$$\frac{\partial \overline{T}}{\partial y} = 0$$
 at $y = 0$ and $y = b$, $0 < x < a$, for $t > 0$

$$\overline{T} = T_0$$
 for $t = 0$, in $0 < x < a$, $0 < y < b$

where

$$\overline{T}(x, y, t) = \frac{1}{c} \int_{z=0}^{c} T(x, y, z, t) dz$$



Reduced models: Linear problem with properties at T^*

Classical Lumped Formulation:

Temperature gradients across the thickness of the plate are fully neglected.

$$T(x, y, 0, t) = T(x, y, c, t) = \overline{T}(x, y, t)$$



Improved Lumped Formulation:

Temperature gradients across the thickness of the plate are not neglected, but taken into account in an approximate form (Cotta, R.M., Mikhailov, M.D., Heat Conduction: Lumped Analysis, Integral Transforms, Symbolic Computation, Wiley-Interscience, New York, USA, 1997.).

H_{1,1} formula (correct trapezoidal rule):
$$\overline{T}(x, y, t) \approx \frac{1}{2} [T(x, y, 0, t) + T(x, y, c, t)] + \frac{c}{12} \left[\frac{\partial T}{\partial z} \Big|_{z=0} - \frac{\partial T}{\partial z} \Big|_{z=c} \right]$$

$$\mathbf{H_{0,0} \ formula \ (trapezoidal \ rule):} \qquad \int_{z=0}^{c} \frac{\partial T(x,y,z,t)}{\partial z} dz = T(x,y,c,t) - T(x,y,0,t) \approx \frac{c}{2} \left[\frac{\partial T}{\partial z} \bigg|_{z=0} + \frac{\partial T}{\partial z} \bigg|_{z=c} \right]$$

$$T(x, y, 0, t) = \overline{T}(x, y, t) - \frac{c}{6k^*}q(x, y)$$
 $T(x, y, c, t) = \overline{T}(x, y, t) + \frac{c}{3k^*}q(x, y)$

$$T(x, y, c, t) = \overline{T}(x, y, t) + \frac{c}{3k^*}q(x, y)$$

In general, the direct problem solution with the complete model took around 7.2 s, while the solution with the reduced model took around 0.09 s of CPU time. 34

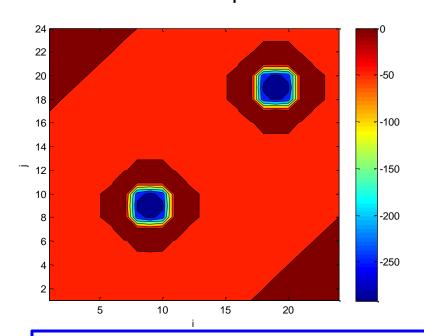


Effects of reduced models

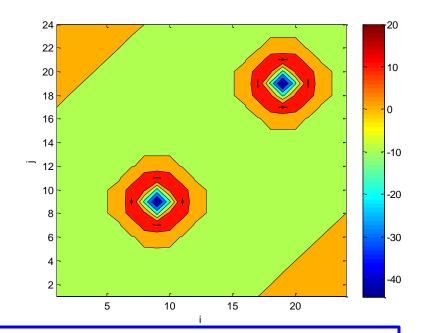
Error of the Direct Problem Solution at the final time:

$$q(x_i, y_j) = \begin{cases} 10^7 W m^{-2} &, \text{ for } 8 \le i \le 10 \text{ and } 8 \le j \le 10 \\ 10^7 W m^{-2} &, \text{ for } 18 \le i \le 20 \text{ and } 18 \le j \le 20 \\ 0 &, \text{ elsewhere} \end{cases}$$

Classical Lumped Model



Improved Lumped Model



Orlande, H.R.B., Dulikravich, G., Inverse Heat Transfer Problems and their Solutions within the Bayesian Framework, ECCOMAS Special Interest Conference, Numerical Heat Transfer 2012, 4-6 September 2012, Gliwice-Wrocław, Poland



SOLUTION OF INVERSE PROBLEMSImprovement of solutions with reduced models

DELAYED ACCEPTANCE METROPOLIS-HASTINGS ALGORITHM

(Christen, J. and Fox, C., Markov chain Monte Carlo Using an Approximation, *Journal of Computational and Graphical Statistics*, vol. 14, no. 4, pp. 795–810, 2005)

- 1. Sample a *Candidate Point* \mathbf{P}^* from a proposal distribution $p(\mathbf{P}^*, \mathbf{P}^{(t-1)})$.
- 2. Calculate the acceptance factor with the surrogate model:

$$\alpha = \min \left[1, \frac{\pi(\mathbf{P}^* \mid \mathbf{Y}) p(\mathbf{P}^{(t-1)}, \mathbf{P}^*)}{\pi(\mathbf{P}^{(t-1)} \mid \mathbf{Y}) p(\mathbf{P}^*, \mathbf{P}^{(t-1)})} \right]$$

- 3. Generate a random value U that is uniformly distributed on (0,1).
- 4. If $U \le \alpha$, proceed to step 5. Otherwise, return to step 1.
- 5. Calculate a new acceptance factor with the complete model:

$$\alpha_c = \min \left[1, \frac{\pi_c(\mathbf{P}^* \mid \mathbf{Y}) p(\mathbf{P}^{(t-1)}, \mathbf{P}^*)}{\pi_c(\mathbf{P}^{(t-1)} \mid \mathbf{Y}) p(\mathbf{P}^*, \mathbf{P}^{(t-1)})} \right]$$

- 6. Generate a new random value U_c which is uniformly distributed on (0,1).
- 7. If $U_c \leq \alpha_c$, set $\mathbf{P}^{(t)} = \mathbf{P}^*$. Otherwise, set $\mathbf{P}^{(t)} = \mathbf{P}^{(t-1)}$.
- 8. Return to step 1.

where $\pi(\mathbf{P}|\mathbf{Y})$ and $\pi_c(\mathbf{P}|\mathbf{Y})$ are the posterior distributions with the likelihoods computed with the surrogate model and with the complete model, respectively.



PRIOR DISTRIBUTIONS Total variation non-informative prior

$$\pi(\mathbf{P}) \propto \exp[-\alpha TV(\mathbf{P})]$$

$$TV(\mathbf{P}) = \sum_{i=2}^{I-1} \sum_{j=2}^{J-1} \Delta y \left[\left| q(x_i, y_j) - q(x_{i+1}, y_j) \right| + \left| q(x_i, y_j) - q(x_{i-1}, y_j) \right| \right] + \Delta x \left[\left| q(x_i, y_j) - q(x_i, y_{j+1}) \right| + \left| q(x_i, y_j) - q(x_i, y_{j-1}) \right| \right]$$

Helcio R. B. Orlande, George S. Dulikravich, Markus Neumayer, Daniel Watzenig, Marcelo J. Colaço, Accelerated Bayesian Inference For The Estimation Of Spatially Varying Heat Flux In A Heat Conduction Problem, *Numerical Heat Transfer – Part A*, In press



SOLUTION OF INVERSE PROBLEMSImprovement of solutions with reduced models

APPROXIMATION ERROR MODEL

- Kaipio, J. and Somersalo, E., *Statistical and Computational Inverse Problems*, Applied Mathematical Sciences 160, Springer-Verlag, 2004
- Kaipio, J., and Somersalo, E., Statistical Inverse Problems: Discretization, Model Reduction and Inverse Crimes, *Journal of Computational and Applied Mathematics*, vol. 198, pp. 493–504, 2007.

In the approximation error model (AEM) approach, the statistical model of the approximation error is constructed and then represented as additional noise in the measurement model [1,19-23]. With the hypotheses that the measurement errors are additive and independent of the parameters \mathbf{P} , one can write

$$\mathbf{Y} = \mathbf{T}_c(\mathbf{P}) + \mathbf{e} \tag{16}$$

where $\mathbf{T}_c(\mathbf{P})$ is the sufficiently accurate solution of the complete model given by equations (1.a-h). The vector of measurement errors, \mathbf{e} are assumed here to be Gaussian, with zero mean and known covariance matrix \mathbf{W} .



APPROXIMATION ERROR MODEL

$$\mathbf{Y} = \mathbf{T}(\mathbf{P}) + [\mathbf{T}_{c}(\mathbf{P}) - \mathbf{T}(\mathbf{P})] + \mathbf{e}$$

By defining the error between the complete and the surrogate model solutions as

$$\boldsymbol{\varepsilon} = [\mathbf{T}_{c}(\mathbf{P}) - \mathbf{T}(\mathbf{P})]$$

equation (17) can be written as

$$\mathbf{Y} = \mathbf{T}(\mathbf{P}) + \mathbf{\eta}$$

where

$$\eta = \varepsilon + e$$

Helcio R. B. Orlande, George S. Dulikravich, Markus Neumayer, Daniel Watzenig, Marcelo J. Colaço, Accelerated Bayesian Inference For The Estimation Of Spatially Varying Heat Flux In A Heat Conduction Problem, *Numerical Heat Transfer – Part A*, In press



APPROXIMATION ERROR MODEL

η is modeled as a Gaussian variable

$$\tilde{\pi}(\gamma, \mathbf{P}|\mathbf{Y}) \propto \gamma^{(II+2)/2} \exp \left\{ -\frac{1}{2} [\mathbf{Y} - \mathbf{T}(\mathbf{P}) - \overline{\mathbf{\eta}}]^T \tilde{\mathbf{W}}^{-1} [\mathbf{Y} - \mathbf{T}(\mathbf{P}) - \overline{\mathbf{\eta}}] - \frac{1}{2} \gamma (\mathbf{P} - \mathbf{\mu})^T \mathbf{\Gamma}^{-1} (\mathbf{P} - \mathbf{\mu}) - \frac{1}{2} \left(\frac{\gamma}{\gamma_0} \right)^2 \right\}$$

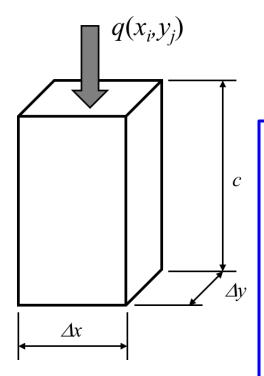
$$\frac{\overline{\eta} \approx \overline{\epsilon}}{\text{Enhanced error model:}} \quad \tilde{\mathbf{W}} \approx \mathbf{W}_{\epsilon} + \mathbf{W}$$

$$\tilde{\mathbf{W}} \approx \mathbf{W}_{\epsilon} + \mathbf{W}$$

Helcio R. B. Orlande, George S. Dulikravich, Markus Neumayer, Daniel Watzenig, Marcelo J. Colaço, Accelerated Bayesian Inference For The Estimation Of Spatially Varying Heat Flux In A Heat Conduction 41 Problem, Numerical Heat Transfer – Part A, In press



SOLUTION OF INVERSE PROBLEMS



Gaussian prior

Energy Balance:
$$q(x_i, y_j) = C^* c \frac{d T(x_i, y_j)}{d t}$$

In order to generate this physically motivated Gaussian prior, and at the same time not violate the Bayesian principle that the prior is the information for the unknowns (coded in the form of probability distribution functions) that is available before the measurements are taken, we assume here that another kind of measurements is also available. Such other kind of measurements is only used to generate the prior, and is considered independent of the temperature measurements used in the inverse analysis, that is, for the computation of the likelihood.

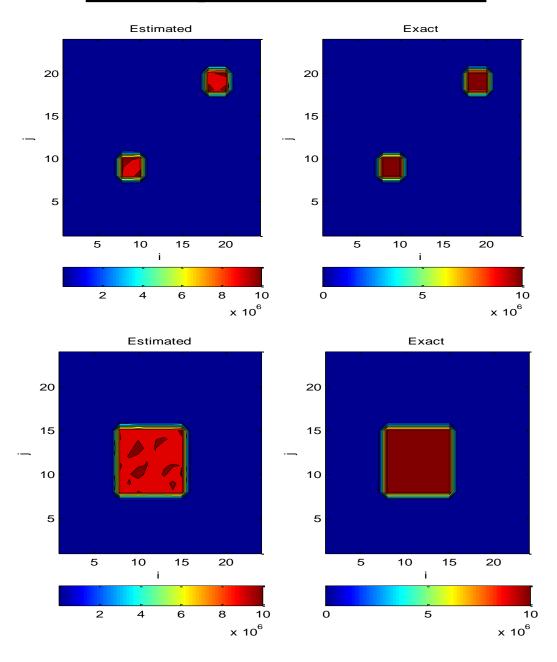


Test case	Flux	Prior	Approach
1	A	TV	-
2	В	TV	-
3	C	TV	-
4	A	TV	DAMH
5	В	TV	DAMH
6	C	TV	DAMH
7	A	Gaussian	-
8	В	Gaussian	-
9	C	Gaussian	-
10	A	Gaussian	AEM
11	В	Gaussian	AEM
12	C	Gaussian	AEM

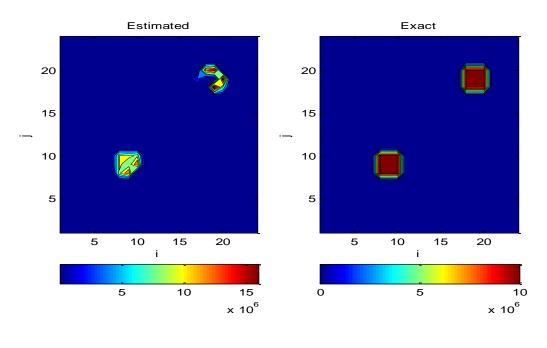


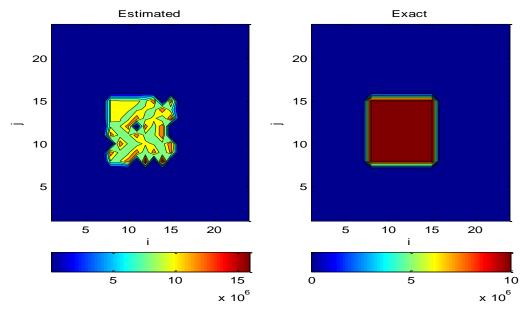
Test	CPU Time	Acceptance ratio (%)	RMS Error (W/m²)
case	(h)		
1	2.7	10.9	$9.3x10^4$
2	2.8	9.0	6.6×10^4
3	2.6	9.9	$1.1x10^5$
4	114.2	46.7 – 5.3	$9.8x10^4$
5	113.0	47.9 – 4.2	$5.9x10^4$
6	98.3	40.8 - 5.9	1.4×10^5
7	2.6	11.3	$9.3x10^4$
8	2.8	9.3	6.6×10^4
9	2.7	10.2	1.1×10^5
10	44.5	12.8	$4.1x10^4$
11	44.2	11.0	$2.6x10^4$
12	42.5	11.2	8.5x10 ⁴
1	2.6	9.1	1.1×10^6
2	2.6	7.5	1.0×10^6
3	2.6	9.1	1.8×10^6
4	98.7	41.9 - 6.8	$1.1x10^6$
5	93.5	44.6 – 5.7	6.9×10^5
6	64.5	34.6 - 5.4	$1.4x10^6$
7	2.7	9.1	1.1×10^6
8	2.6	8.3	$9.8x10^5$
9	2.6	9.4	$1.3x10^6$
10	42.9	9.8	$1.2x10^6$
11	43.3	11.9	$1.2x10^6$
12	43.1	8.7	$2.0x10^6$

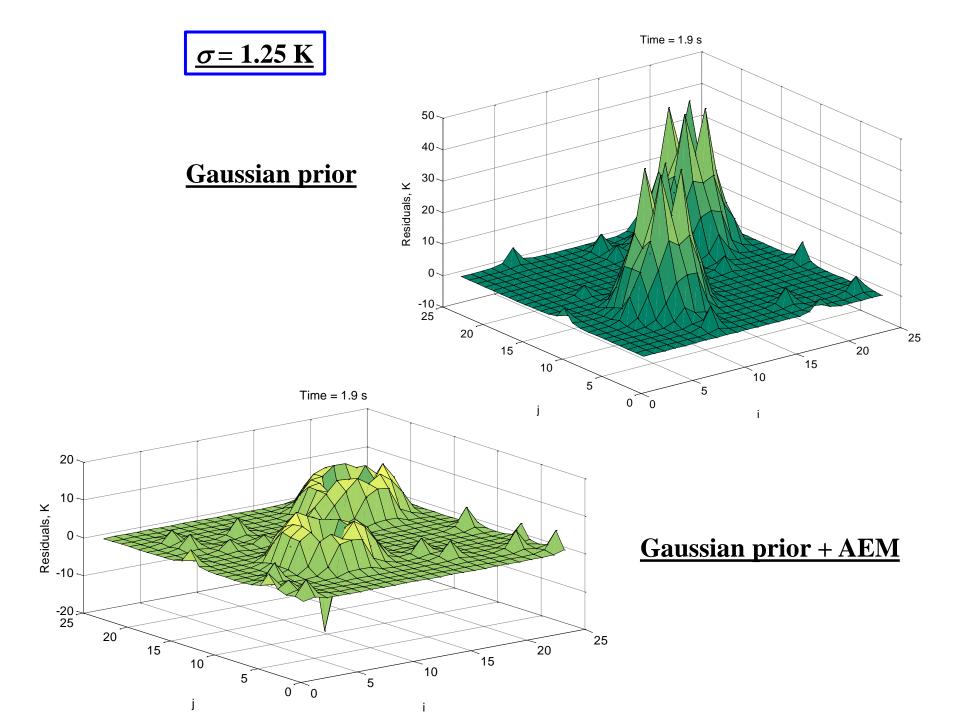
Gaussian prior + AEM - σ = 0.02 K



TV prior + DAMH - σ = 1.25 K

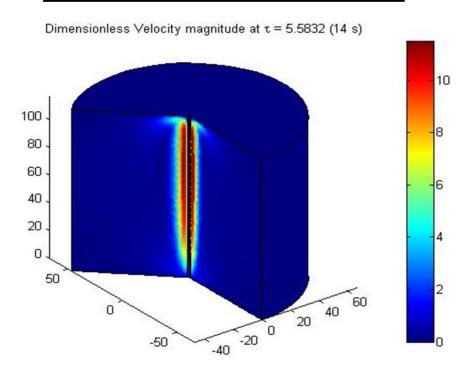








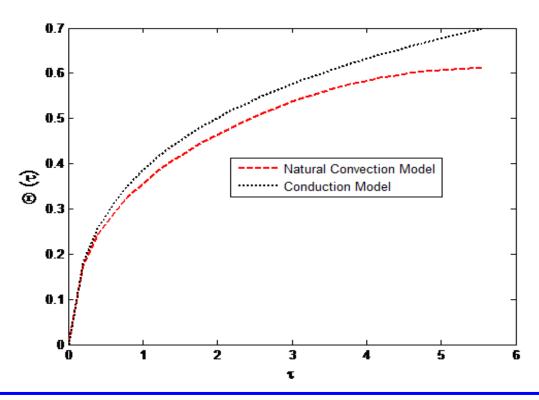
CONVECTIVE EFFECTS IN LIQUIDS CHARACTERIZED BY THE LINE HEAT SOURCE PROBE



Bernard Lamien, Helcio R. B. Orlande, Approximation Error Model To Account For Convective Effects In Liquids Characterized By The Line Heat Source Probe, *4th Inverse Problems, Design and Optimization 48 Symposium (IPDO-2013)*, Albi, France, June 26-28, 2013



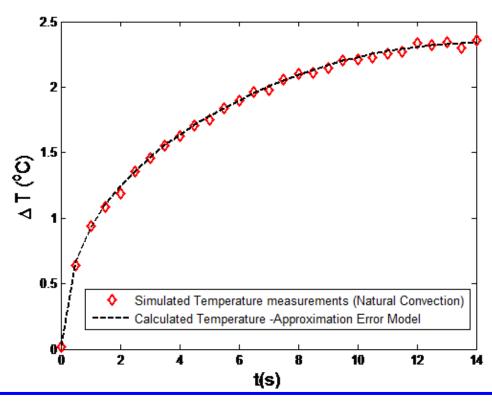
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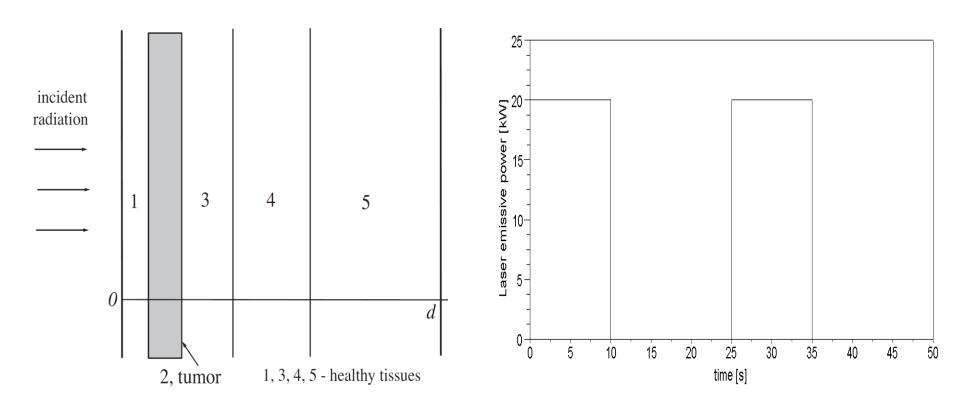
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HYPERTHERMIA TREATMENT OF CANCER - NANOPARTICLES



Leonid A. Dombrovsky, Victoria Timchenko, Michael Jackson, Guan H. Yeoh, A combined transient thermal model for laser hyperthermia of tumors with embedded gold nanoshells, *International Journal of Heat and Mass Transfer*, Volume 54, Issues 25–26, December 2011, Pages 5459–5469



COMPLETE MODEL FOR THE FLUENCE RATE

$$\nabla \cdot \left[-D^*(\mathbf{r}) \nabla \Phi_d(\mathbf{r}) + \frac{\sigma_s^*(\mathbf{r}) g^*(\mathbf{r})}{\mu_{tr}^*(\mathbf{r})} \Phi_c(\mathbf{r}) \mathbf{i} \right] + \sigma_a(\mathbf{r}) \Phi_d(\mathbf{r}) = \sigma_s^*(\mathbf{r}) \Phi_c(\mathbf{r})$$

$$\mathbf{n} \cdot \left(-D(\mathbf{r})\nabla \Phi_d(\mathbf{r}) + \frac{\sigma_s^*(\mathbf{r})g^*(\mathbf{r})}{\mu_{tr}^*(\mathbf{r})}\Phi_c(\mathbf{r})\mathbf{i}\right) + \frac{1}{2A}\Phi_d(\mathbf{r}) = 0$$

Where $\Phi_c(\mathbf{r})$ is given by Beer Law

$$\sigma_s^* = \sigma_s \left(1 - g^2 \right) \qquad g^* = \frac{g}{1 + g}$$

$$\mu_{tr} = \sigma_a + \sigma_s \left(1 - g \right) \qquad D = 1/3 \mu_{tr} \quad A = \frac{1 - r_{id}}{1 + r_{sd}}$$



REDUCED MODEL FOR THE FLUENCE RATE

Semi-infinite medium irradiated by a wide collimated beam with refractive index mismatched boundaries - Welch, (2011)

$$F_{+}(z) = \frac{S_{+} - r_{id} S_{-}}{(\mu_{t}^{2} - \mu_{eff}^{2})(1 - r_{id})} \exp(-\mu_{eff} z) - \frac{S_{+}}{(\mu_{t}^{2} - \mu_{eff}^{2})} \exp(-\mu_{t} z)$$

$$F_{-}(z) = \frac{q(S_{+} - r_{id}S_{-})}{(\mu_{t}^{2} - \mu_{eff}^{2})(1 - r_{id})} \exp(-\mu_{eff}z) - \frac{S_{-}}{(\mu_{t}^{2} - \mu_{eff}^{2})} \exp(-\mu_{t}z)$$

Where
$$S_{+} = (\mu_{s} / 4) [(5 + 9g) \mu_{a} + 5\mu_{s}]$$

$$S_{-} = (\mu_s / 4) \left[\left(1 - 3g \right) \mu_a + \mu_s \right]$$

$$q = \left(\mu_{eff} - 2\mu_a\right) / \left(\mu_{eff} + 2\mu_a\right)$$

The total fluence rate is given as:

$$\Phi_{t}(z) = 2 \left[F_{+}(z) + F_{-}(z) \right] + \Phi_{c}(z)$$



BIOHEAT TRANSFER EQUATION

$$\rho(\mathbf{r},t)c(\mathbf{r},t)\frac{\partial T(\mathbf{r},t)}{\partial t} = k_c(\mathbf{r},t)\nabla T(\mathbf{r},t) + Q_{bio}(\mathbf{r},t) + Q_{laser}(\mathbf{r},t)$$

$$T(r,t) = T_b$$

$$k_c(\mathbf{r},t)\frac{\partial T(\mathbf{r},t)}{\partial \mathbf{r}} + hT(\mathbf{r},t) = hT_b$$

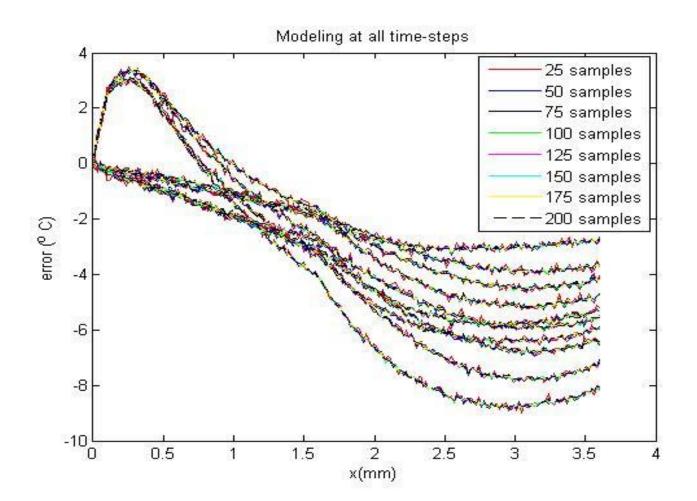
$$T(r,t) = T_b, t > 0$$

$$Q_{laser}(\mathbf{r},t) = \sigma_a(r)\Phi_t(r,t)$$

$$Q_{bio}(\mathbf{r},t) = \rho_b(\mathbf{r},t)c_b(\mathbf{r},t)v_b(\mathbf{r},t)[T(\mathbf{r},t) - T_b(\mathbf{r},t)] + Q_m(\mathbf{r},t)$$

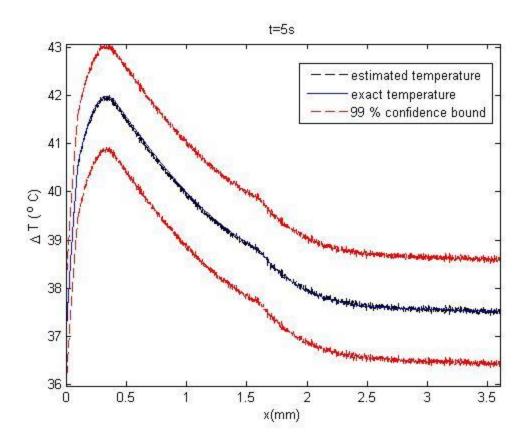


CONVERGENCE ANALYSIS OF THE MODELING ERROR



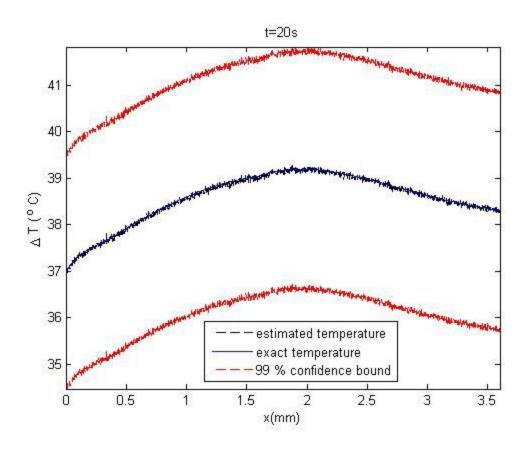


ESTIMATED TEMPERATURE – PARTICLE FILTER ASIR+AEM (sensor at x=0.5 mm)



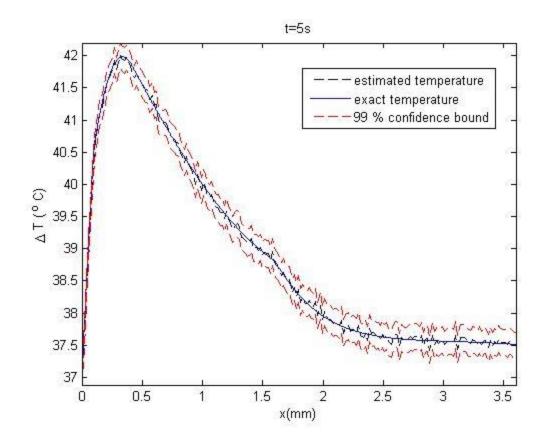


ESTIMATED TEMPERATURE – PARTICLE FILTER ASIR+AEM (sensor at x=0.5 mm)



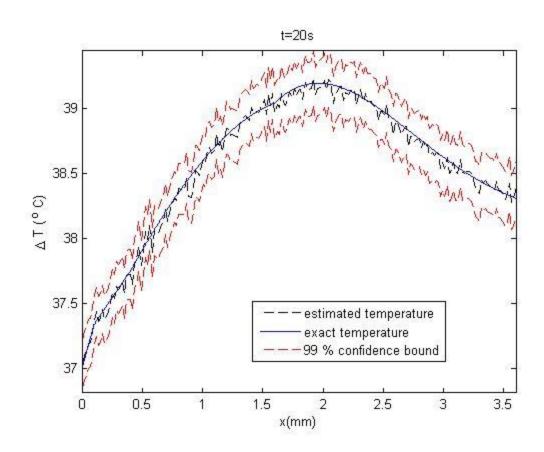


ESTIMATED TEMPERATURE – PARTICLE FILTER ASIR+AEM (sensor at x=1.5 mm)





ESTIMATED TEMPERATURE – PARTICLE FILTER ASIR+AEM (sensor at x=1.5 mm)





CONCLUSIONS

• With the recent advancement of fast and affordable computational resources, sampling methods have become more popular within the community dealing with the solution of inverse problems. These methods are backed up by the statistical theory within the Bayesian framework, being quite simple in terms of application and not restricted to any prior distribution for the unknowns or models for the measurement errors.



CONCLUSIONS

- If the number of unknowns is too large, thus requiring a large number of samples to represent the posterior distribution, or the solution of the direct problem is too expensive in terms of computational time, the application of sampling methods may still be prohibitive nowadays.
- The use of surrogate models or response surfaces for the solution of the direct problem are useful for the reduction of the computational time, specially if used with the Approximation Error Approach.
- More efficient sampling algorithms are under development, e.g., the Delayed Acceptance Metropolis-Hastings algorithm.



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